

AMS 02 RADIATORS MASS REDUCTION

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OHB-System

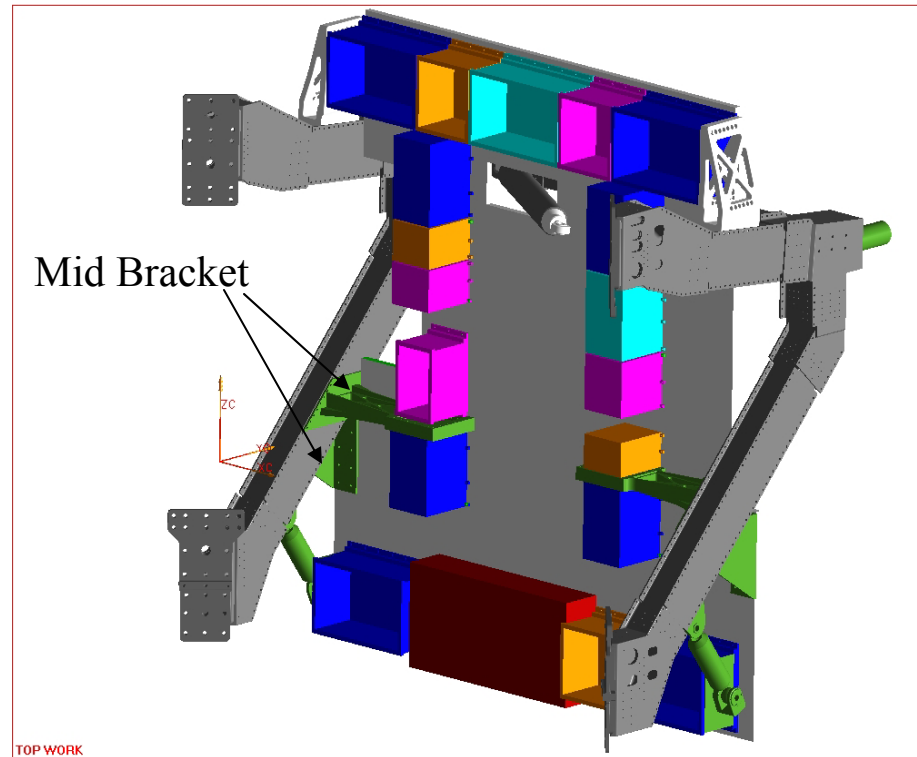
Mid Bracket Design

One of the major design driver is the radiator panel insert load as a result of enforced interface displacements (coupled load analysis)

An approach to reduce the effects of enforced interface displacement is to minimise the constrained DOF's

The current design has:

- 2 x 6 DOF at upper bracket I/F
- 4 x 6 DOF at mid bracket I/F
- 2 x 1 DOF at lower bracket I/F



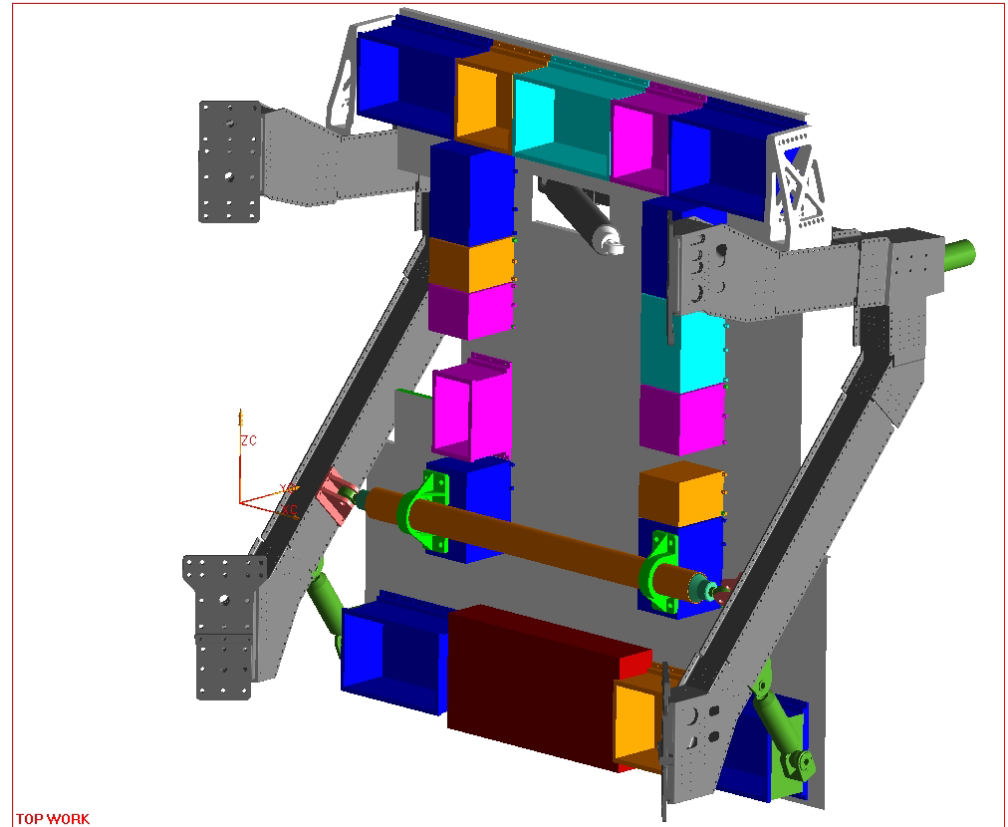
Mid Bracket Design

Alternate mid bracket design:

- A tube integrated between the USS bars with spherical bearing at both ends
- Two clamps attached to the crates forming the interface to the tube
- Additionally one of the upper brackets is released in x-direction

The alternate design has:

- 1 x 6, 1 x 5 DOF at upper bracket I/F
- 1 x 3, 1 x 2 DOF at mid bracket I/F
- 2 x 1 DOF at lower bracket I/F

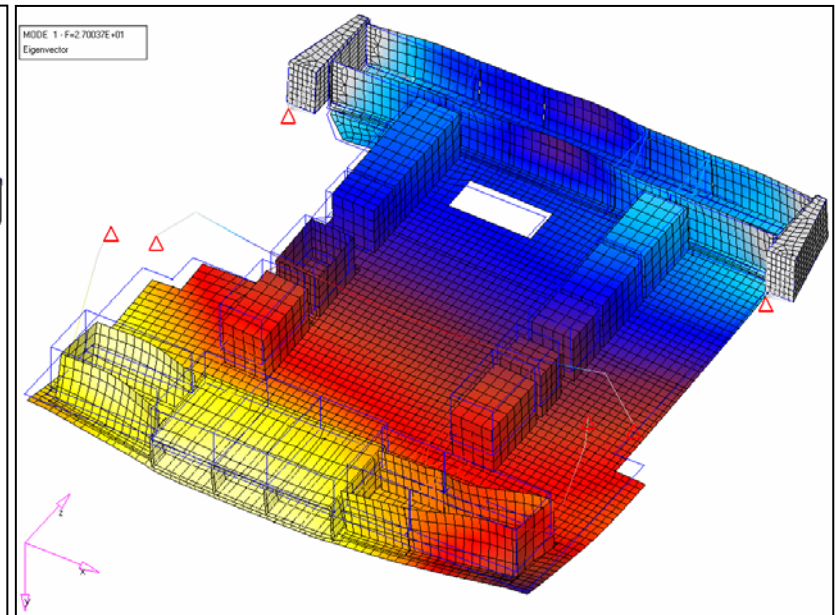
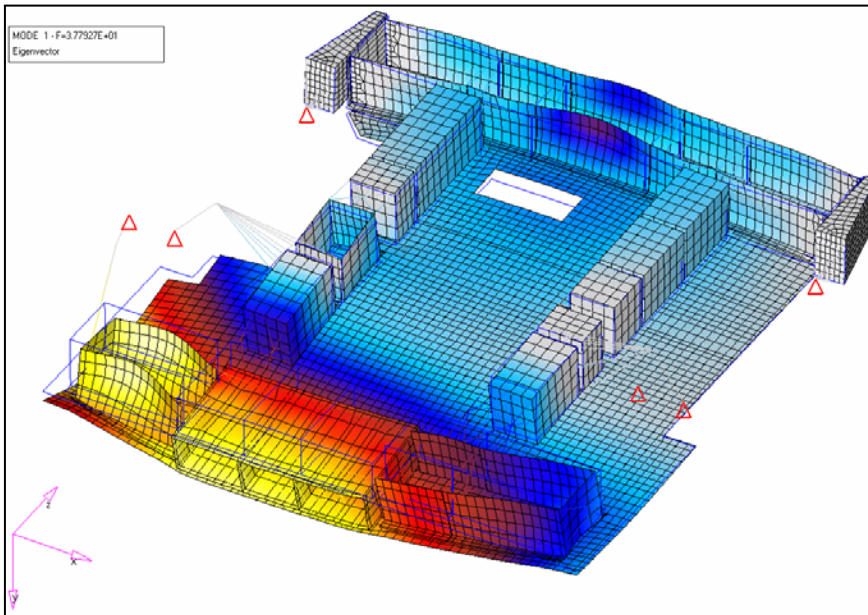


Mid Bracket Design

Natural Frequency

Current Design: $f_1 = 37.7$ Hz

Alternate Design: $f_1 = 27.0$ Hz



Mid Bracket Design

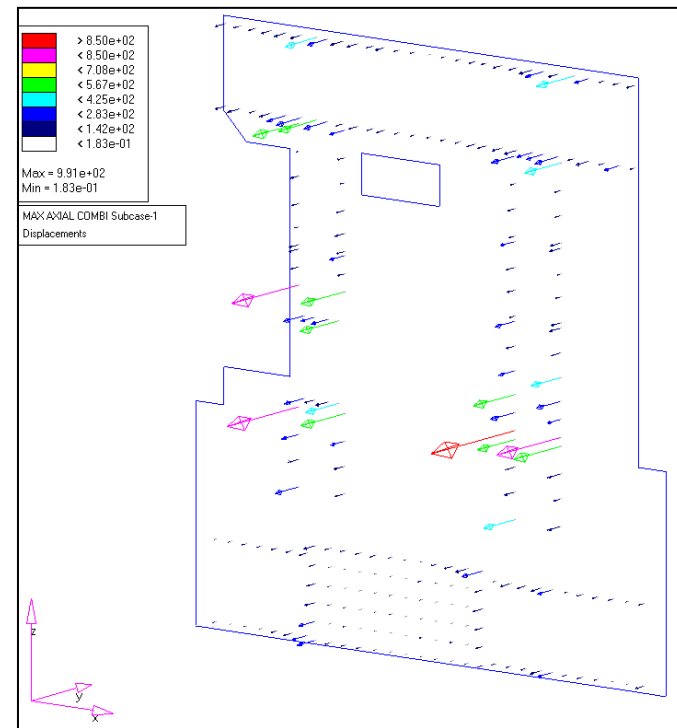
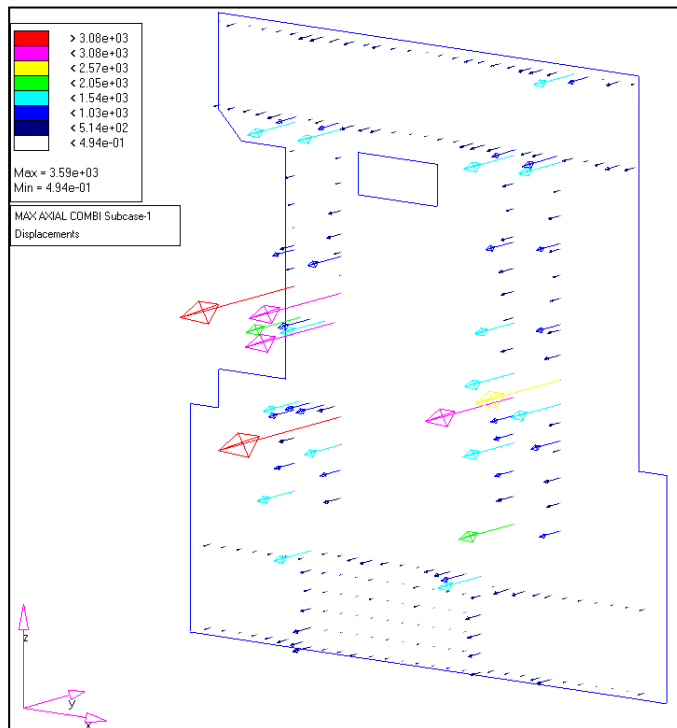
Sandwich Insert max. Axial Load

Current Design:

max. insert axial load $F_{amax} \approx 3600$ N

alternate Design:

max. insert axial load $F_{amax} \approx 1000$ N

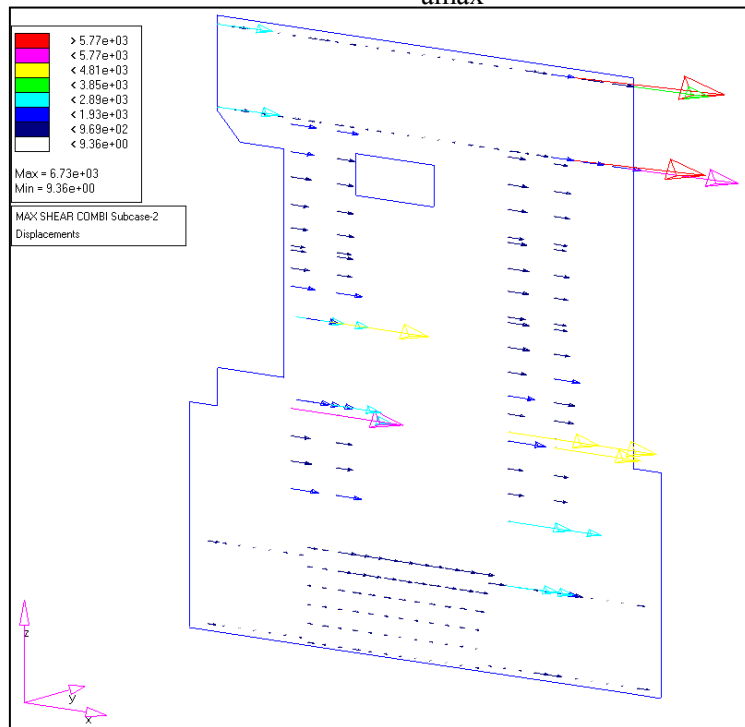


Mid Bracket Design

Sandwich Insert max. Shear Load

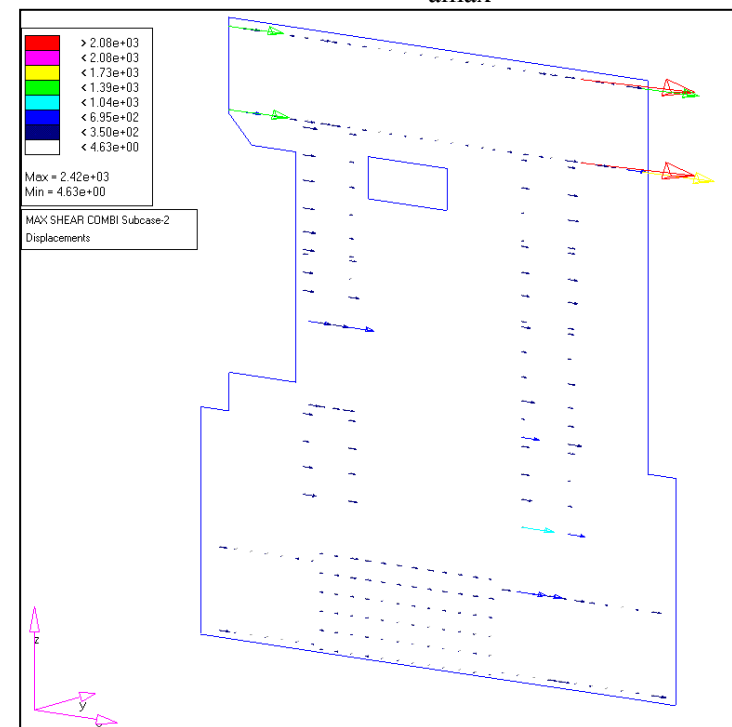
Current Design:

max. insert shear load $F_{amax} \approx 6700$ N



alternate Design:

max. insert shear load $F_{amax} \approx 2400$ N



Mid Bracket Design

Mid Bracket Mass Estimate

Current Design:

$m_{\text{total}} \approx 19 \text{ kg}$ (from FE-Model)

Alternate Design: Aluminum

$m_{\text{tube}} \approx 6 \text{ kg}$

$m_{\text{brackets}} \approx 5 \text{ kg}$

$m_{\text{total}} \approx 11 \text{ kg}$

Mass saving: $\approx 8 \text{ kg}$

Alternate Design: CFRP

$m_{\text{tube}} \approx 4 \text{ kg}$

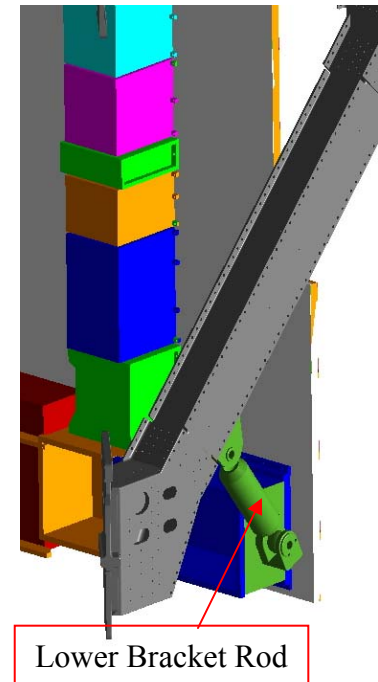
$m_{\text{brackets}} \approx 3 \text{ kg}$

$m_{\text{total}} \approx 7 \text{ kg}$

Mass saving: $\approx 12 \text{ kg}$

Mass Reduction of Lower Bracket (ROD)

Current Design					Alternative 1 (reduced tube cross section)					Alternative 2 (CFRP Tube)				
Material / Safety Factor	Material	-	-	7075	Material	-	-	7075	Material	-	-	CFRP		
	youngs module	E	N/mm ²	71000	youngs module	E	N/mm ²	71000	youngs module	E	N/mm ²	100000		
	ultimate strength	σ_u	N/mm ²	414	ultimate strength	σ_u	N/mm ²	414	ultimate strength	σ_u	N/mm ²	700		
	yield strength	σ_y	N/mm ²	324	yield strength	σ_y	N/mm ²	324	yield strength	σ_y	N/mm ²	N/A		
	Safety Factor ultimate	ju	-	2.00	Safety Factor ultimate	ju	-	2.00	Safety Factor ultimate	ju	-	2.00		
Safety Factor yield	jy	-	1,25	Safety Factor yield	jy	-	1,25	Safety Factor yield	jy	-	1,25			
Density	rho	kg/mm ³	2,80E-06	Density	rho	kg/mm ³	2,80E-06	Density	rho	kg/mm ³	1,60E-06			
Geometry	total length	l _k	mm	354	total length	l _k	mm	354	total length	l _k	mm	354		
	tube length	l _{tube}	mm	194	tube length	l _{tube}	mm	194	tube length	l _{tube}	mm	194		
	outer Diameter	Da	mm	80	outer Diameter	Da	mm	25	outer Diameter	Da	mm	25		
	inner Diameter	Di	mm	70	inner Diameter	Di	mm	22	inner Diameter	Di	mm	23		
	cross section	A	mm ²	1178	cross section	A	mm ²	111	cross section	A	mm ²	75		
moment of inertia	I	mm ⁴	832031	moment of inertia	I	mm ⁴	7676	moment of inertia	I	mm ⁴	5438			
max compression force	F _c	N	20000	max compression force	F _c	N	20000	max compression force	F _c	N	20000			
Strength	Tube stress	σ_c	N/mm ²	17,0	Tube stress	σ_c	N/mm ²	180,6	Tube stress	σ_c	N/mm ²	265,3		
	Margin of Safety ultimate	M _{su}	-	11,2	Margin of Safety ultimate	M _{su}	-	0,15	Margin of Safety ultimate	M _{su}	-	0,32		
	Margin of Safety yield	M _{sy}	-	14,3	Margin of Safety yield	M _{sy}	-	0,44	Margin of Safety yield	M _{sy}	-	N/A		
Buck	critical buckling force	F _{buck}	$\pi^2 E^* I / k^2$	4652551	critical buckling force	F _{buck}	$\pi^2 E^* I / k^2$	42921	critical buckling force	F _{buck}	$\pi^2 E^* I / k^2$	42829		
	Margin of Safety buckling	M _{sb}	-	115	Margin of Safety buckling	M _{sb}	-	0,07	Margin of Safety buckling	M _{sb}	-	0,07		
Mass of Tube (2x)	m _t	kg	1,280	Mass of Tube (2x)	m _t	kg	0,120	Mass of Tube (2x)	m _t	kg	0,047			

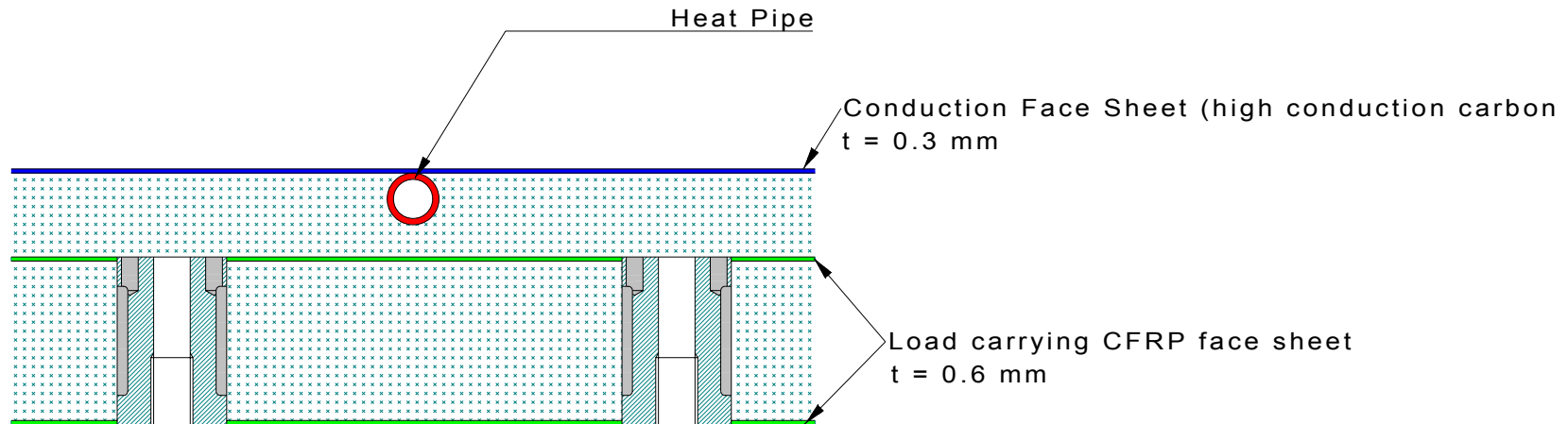


1. Rod tube made of Aluminum with reduced cross section could save a mass of ~ 1.1 kg
2. Rod tube made of CFRP with an additional reduction of cross section saves ~ 1.2 kg

Further mass reduction can be realized when smaller spherical bearings are used:

- MS14103-06 with inner diameter of 9.5 mm instead of 35 mm (F_{u-radial} = 60.000 N)
- Additionally bracket dimension could be reduced significantly in this case

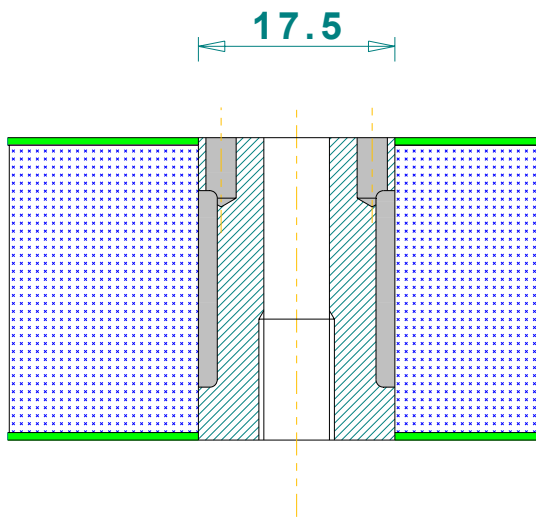
Mass Reduction Zenith Radiator



- Current design with aluminum face sheets
 - Alternative design with CFRP face sheets could save a mass of ~10 kg
- Detailed Analyses (thermal and structural) are required

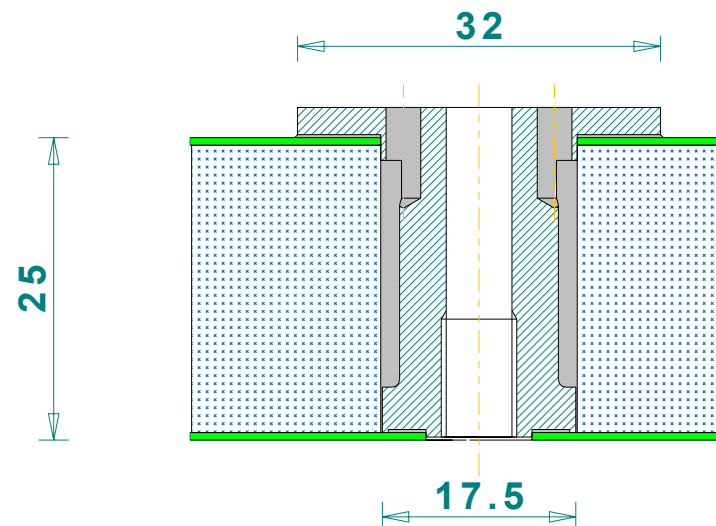
Sandwich Inserts

Standard Insert



Allowable load from
ESA PSS-03-1202
- PSS = 1000 N
- QSS = 2800 N

Modified Insert



Allowable load to be determined
by detailed analysis and/or test

For a smaller insert (M5)
we measured:

PSS = 2800 N

QSS: not tested

Conclusion:

Using the modified insert, we can increase
the load carrying capability significantly.
In order to perform a reliable analytical
verification, static tests should be carried
out beforehand.

